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## 4. Investigation of a CTS Solar Cell Test Patch Under Simulated Geomagnetic Substorm Charging Conditions

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## Abstract

The **CTS** solar array technology experiment which consists of a solar cell test patch on the Kapton-substrate solar array and the appertaining electronics unit has **been** operating in geostationary orbit for nearly 1 year without any malfunction although it is expected to be strongly influenced by charging effects on the array surface.

The results of a post-launch test program show that the experiment would not survive a discharge due to electrostatic charging in the test patch area. In a simulated substorm, environment discharges were obtained only below a temperature threshold of about 30°C. With solar illumination, this threshold is reduced below 0°C.

## 1. INTRODUCTION

Spacecraft in geosynchronous orbit find under magnetic substorm conditions are known to be subject to differential charging of different material surfaces leading to high values of electric stress and arc discharges if the threshold for electrical breakdown is surpassed. The highest electric stress is expected on

insulating material surfaces which are not sun-illuminated and therefore cannot equilibrate at low potentials by photoemission of electrons.

The Communications Technology Satellite, CTS, which has been in orbit since January 1976 has a sun-oriented 2-wing solar array using a 75 micron thick kapton-glass fibre-compound flexible substrate. The insulating rear side of the array is shaded permanently and therefore constitutes a principal source of discharges.

The CTS flexible solar array is equipped with a solar cell test patch which forms part of the solar array technology experiment provided by ESTEC. The test patch and the appertaining electronics unit are expected to be strongly influenced by discharges on the solar array surface. Therefore, a post-launch test program was initiated in order to study the behaviour of the solar array electronics experiment under simulated substorm conditions. The tests described here were performed in the 2.5 m Space Simulation Chamber of DFVLR in Porz wahn, Germany, in the first quarter of 1976.

## 2. TEST OBJECTIVES

The data which are presently available on differential charging are discharges are not sufficient to predict the behaviour of the CTS solar array experiment in a geomagnetic substorm for two reasons:

- (1) Most of the investigations have been done on materials level and the results cannot be applied to more complex structures because there is too little knowledge on structural and size effects.
- (2) The investigations on representative samples<sup>1</sup> have not been performed in a representative environment, as far as solar simulation and temperature are concerned.

Therefore a principal goal of the investigation was to analyze the influence of simulated substorm electron plasmas on a representative solar cell test patch under representative environmental conditions.

In detail, the test objectives were as follows:

- (1) Measurement of the electron beam induced leakage current through the substrate as a function of electron energy, ambient temperature and solar illumination.
- (2) Analysis of the discharge pulse frequency and pulse shape at the output of the solar cell test patch as a function of temperature and solar illumination.
- (3) Analysis of the AEE (array experiment electronics) performance in simulated substorm.

The outcome of these measurements would allow for direct conclusions in conjunction with actual flight data:

(1) If characteristic anomalies occur at the AEE output during arc discharging, then the AEE could be used as a discharge indicator on CTS. Similarly, if arc discharges turn out to destroy the AEE, one could determine the time of the first substorm generated discharge pulse from the time of malfunction of the AEE.

(2) If the solar array experiment performance is not disturbed by discharge pulses, one can have more confidence in the reliability of the flight data.

### 3. THE SUBSTORM SIMULATION FACILITY

The large 2.5 m space simulation chamber at DFVLR, Porz wahq Germany, was selected because boundary effects from the wall chambers are kept to a minimum, and because it offers the possibility to mount much larger test samples in a future series of tests.

A cross section through the chamber is shown in Figure 1. The sample is mounted vertically by means of teflon wires. Illumination of the sample front side is provided by a sun simulator of 1 solar constant. The sample rear side can be irradiated homogeneously with electrons, the electron gun being mounted on the center flange of the chamber lid at the rear side. Visual control is possible through a window inclined  $15^\circ$  to the beam axis.

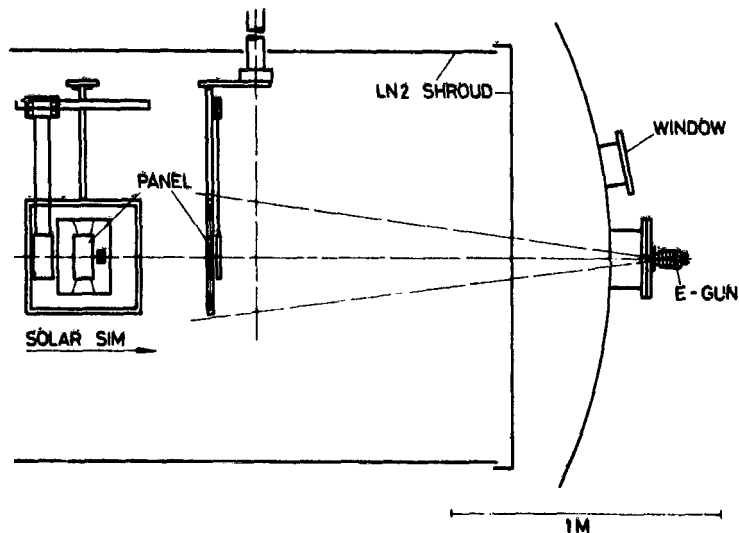


Figure 1. The Geomagnetic Substorm Simulation Facility

Using the liquid nitrogen cold shroud, the residual pressure is below  $10^{-6}$  torr. Without cold shroud, the pressure is between  $10^{-4}$  and  $10^{-5}$  torr.

The electron energy can be continuously varied between 0 and 60 kV. The current density at an electron beam diameter of  $1\text{ m}^2$  in the test plane is between 1 and  $100\text{ nA/cm}^2$ .

The uniformity of the electron beam intensity in the test plane can be checked using a detector with an array of six equally sized receiver plates. A beam uniformity of  $\pm 30$  percent is achieved without special adjustments.

#### 4. TEST SAMPLE

The test specimen consisted of two parts: the solar cell test patch on a flexible panel-substrate and the AEE engineering unit.

The layout of the test patch is shown in Figure 2. Three solar cells are arranged in parallel and 9 cells in series. On the right hand side is a representative part of the CTS solar array wiring. At the bottom two PT-temperature sensor are positioned beneath two dummy cells.

The substrate consists of a compound of:

25  $\mu\text{m}$  kapton H film

35  $\mu\text{m}$  glass fibre cloth

5  $\mu\text{m}$  polyester adhesive (Dupont 46971)

The solar cells are mounted on the glass fiber side with RTV 560.

Typical I-V characteristics of the test patch under 1 solar constant illumination and at various temperatures are shown in Figure 3.

The AEE has the function to monitor the performance of the test patch in orbit. The parameters to be monitored are:

- (1) the open Circuit voltage  $V_{oc}$ ,
- (2) the short circuit current  $I_{sc}$ ,
- (3) current and voltage at four points of the I-V curve determined by resistors  $R_1 - R_4$  (see Figure 3), and
- (4) temperatures at the test patch and at four other positions of the panel.

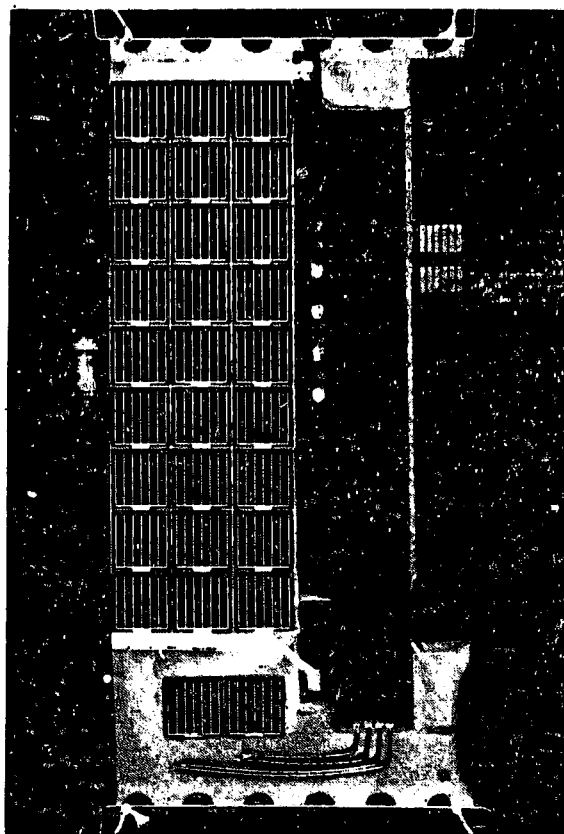


Figure 2. The CTS Solar Cell test Patch

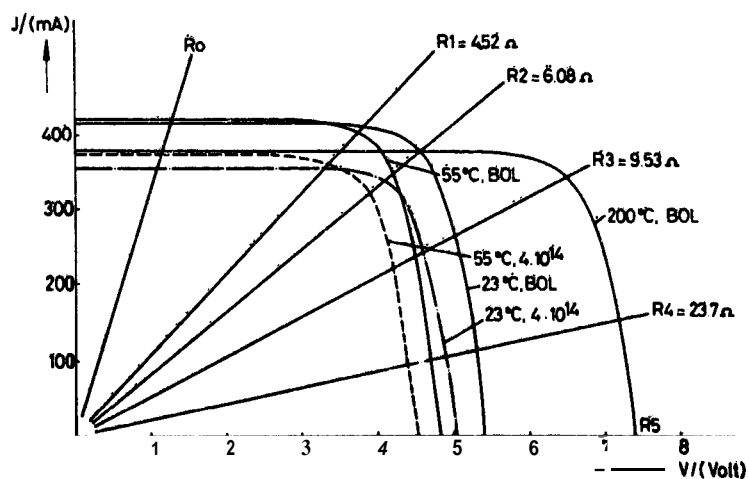


Figure 3. Test Patch I-V Curves

## 5. CHARACTERISTICS OF DISCHARGE PULSES

With the test patch at room temperature and no illumination, discharges were observed at electron energies above 15 kV.

The discharge frequency was found to be proportional to the electron beam current density. At a beam current of  $60 \text{ nA/cm}^2$  a discharge rate of 8 pulses/min was measured, the pulses occurring at rather regular intervals.

Visual observation of the test patch during discharges showed a localized spot of high intensity light emission surrounded by a lower intensity 'Lichtenberg-figure' covering the whole sample rearside. The position of the high intensity spot varied from discharge to discharge and no preferred position could be detected.

To analyze the electrical characteristics of discharges as seen at the test patch terminals, the test patch was connected to an external circuitry as shown in Figure 4. The length of the connecting leads corresponded approximately to the wiring on the spacecraft in order to simulate in-orbit conditions to a certain extent. Nevertheless, considerable deviations in the high frequency properties were anticipated due to different capacitive and inductive components.

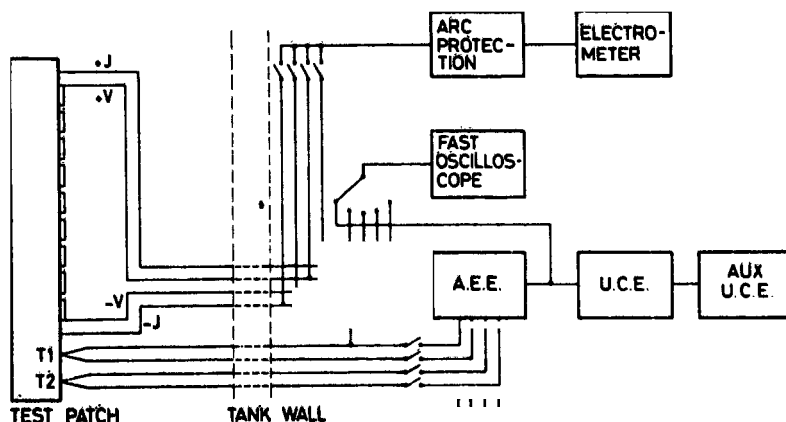


Figure 4. Wiring Diagram

A  $20 \text{ k}\Omega$  terminal resistor, consisting of  $20 \Omega + 180 \Omega + 1800 \Omega$  in series, was connected across the output of the  $3 \times 9$  solar cell module. This corresponds to the input impedance of the AEE when connected to the test patch. Transient signals during discharge were measured at the  $0 \Omega$ ,  $20 \Omega$ , and  $200 \Omega$  points of the terminal resistor using a Tektronix 7704-A oscilloscope with a 10:1 attenuator. The peak voltages obtained were:

2 V at 0  $\Omega$  (EMI)  
 10 - 20 V at 20  $\Omega$   
 100 - 200 V at 200  $\Omega$

From this, the extrapolated peak voltage at 2 K $\Omega$  would be 1 - 2 kV.

The transient pulses were recorded using a 2048 channel biomation transient recorder with a 50  $\Omega$  input impedance and a channel width of 10  $\mu$ sec. Typical recordings are shown in Figure 5. The initial portion of the signal is not displayed in full amplitude due to the voltage limitation of the recorder to  $\pm 5$  volts. As can be seen, the pulses consist of damped oscillations with a typical decay time of 3-5  $\mu$ sec for a terminal resistor of 50  $\Omega$ .

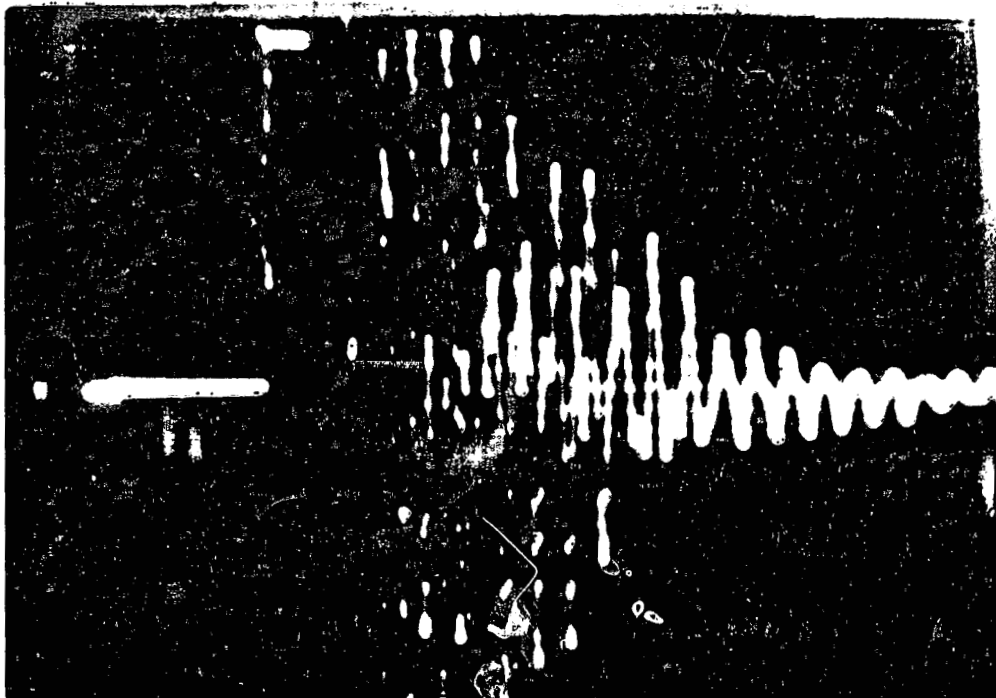


Figure 5. Discharge Transient Pulse (x-axis : 2  $\mu$ sec/div; y-axis : 1.25 V/div)

The high frequency (  $\geq 3$  MHz) oscillations are considered to be strongly influenced by the external circuitry and no direct conclusions can be drawn which are applicable to in-orbit behaviour.

The pulse decay time, however, can be correlated with the RC time of the circuit consisting mainly of the solar cell capacitance of about 70 nF and the terminal resistor of 50  $\Omega$  and 2 k $\Omega$ , respectively. With the 2 k $\Omega$  terminal resistor, the peak voltage was 1000-2000 volt, From  $E_s = 1/2 CU^2$ , a pulse energy of about 166 mJoule is calculated.

It must be kept in mind that pulses of this energy occur at the solar cell test patch output due to pick-up from the energy of the discharge pulse at the rear side of the test patch. The maximum energy of the primary discharge pulse can be calculated on the assumption that the test patch represents a plate capacitor negatively charged over the whole rear side surface with respect to the solar cells on the front side which are on ground potential. The total capacitance of this plate capacitor is

$$C = \epsilon \epsilon_0 F/d \approx 4 \text{ nF} .$$

If the entire surface charge is discharged within one discharge pulse, then the total discharge energy would be at maximum

$$E_D = 450 \text{ mJoule} .$$

Comparing  $E_D$  with  $E_s$  and bearing in mind that  $E_s$  is only a fraction of  $E_D$  because only a fraction of the total energy is picked up by the solar cell module, the two energy figures indicate that, in fact, the charge accumulated over the whole rear surface is discharged in one pulse.

This is confirmed by the observed discharge rate of 8 pulses/min at the beam current density of 60 nA/cm<sup>2</sup>. From these figures it can be concluded that the maximum charge deposited on the whole rear surface of about 100 cm<sup>2</sup> area in between two pulses in about 40  $\mu$ A sec which at 15 kV represents a maximum stored energy

$$E_c = Q \cdot U \approx 600 \text{ mJoule} .$$

As part of the charge is lost by secondary emission and conduction,  $E_D$  has to be somewhat smaller than  $E_c$ .

## 6. INFLUENCE OF AMBIENT TEMPERATURE AND ILLUMINATION OF THE DISCHARGE FREQUENCY

During these tests the discharges were monitored using the electron beam detector as receiver antenna. The beam current density was kept between 20 and



$100 \text{ nA/cm}^2$ . Discharges on the test patch rearside caused a steep spike in the beam current recording sufficient for event counting purposes.

**Regular** discharges at normal rates (Section 5) were observed in the dark at room temperature. After opening the solar simulator shutter and exposing the front side of the test patch to one solar constant illumination the discharge activity ceased within less than a minute. No discharges were observed under illumination for time periods of more than 20 min and electron energies up to 20 keV. After turning off the illumination, it took about 3 min until the discharges occurred again.

**Under** illumination the temperature of the test patch as measured with the two temperature sensors rises to about  $100^\circ\text{C}$  with an initial slope of  $40^\circ\text{C/min}$ . Cool-down to ambient temperature after turn-off of the simulator takes about 5 min with an initial slope of  $30^\circ\text{C/min}$ .

The different behavior at turn-on and turn-off indicates that the temperature of the test patch has a strong influence on the discharge frequency. An additional influence of the illumination can, however, not be precluded.

A more detailed examination of the test patch showed that illumination of the front side causes also the rearside to be illuminated because light penetrates the gaps between solar cells into the substrate where it is scattered by the light-pipe action of the glass fiber over the whole rear surface. Photoemission from rearside could therefore prevent excessive charging of the rear surface. Another potential explanation would be photoconduction through the substrate.

To further investigate the influence of illumination, the tests were repeated with the cell gaps covered by a blackened Teflon mask inhibiting the penetration of light to the substrate. Figure 6 shows the discharge frequency before, during, and after solar illumination. The corresponding temperature profile is shown in the upper part. The same behavior as in the test without mask was found, that is, no discharge immediately after turn-on and delayed reoccurrence of discharges after turn-off of illumination.

These results indicate that the test patch temperature is mainly responsible for the ceasing of discharge under illumination.

To verify these results under representative conditions, the tests were repeated at liquid nitrogen ambient temperatures. The results are shown in Figure 7. In the dark the temperature is below  $-150^\circ\text{C}$ . With 1 solar constant illumination the measured temperature rises to about  $50^\circ\text{C}$ . This measured temperature, however, is not identical to the solar cell test patch temperature because the sensors are located beneath two dummy solar cells at the edge of the test patch. Therefore, there is a tendency for measuring the temperature low due to the 'fin-effect' at the test patch edge. This could account for  $-5^\circ\text{C}$  to  $-10^\circ\text{C}$ . On the other hand, there

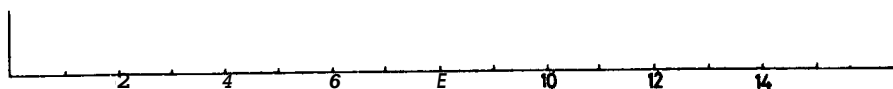


Figure 6. Discharge Rate During Illumination Transient (Without Cooling)

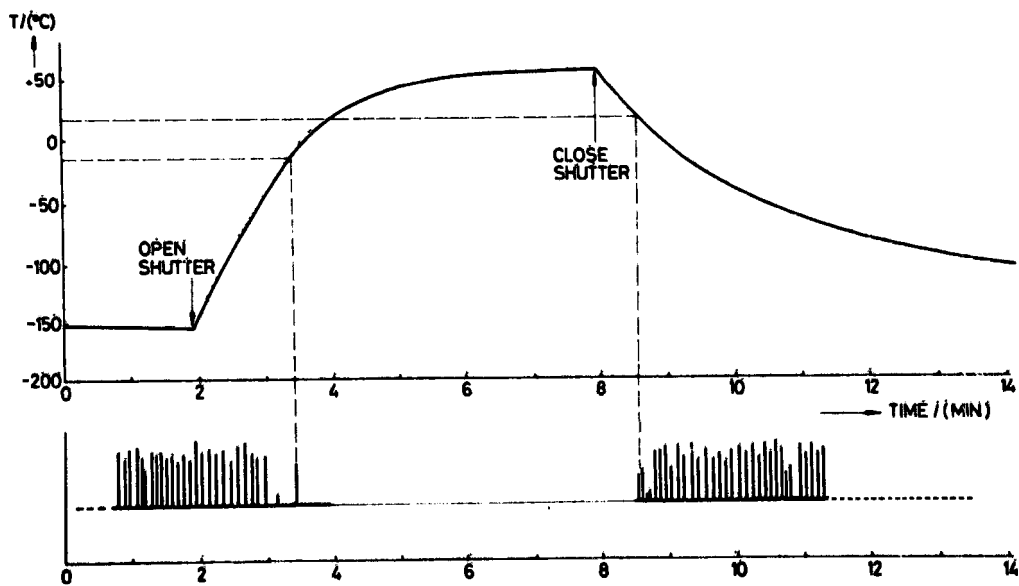


Figure 7. Discharge Rate During Illumination Transient (With  $\text{LN}_2$  Cooling)

is a tendency to measure the temperature about  $10^{\circ}\text{C}$  too high because the solar cells of the module were loaded at maximum power in contrast to the cells on top of the sensors which were in open circuit.

At  $-150^{\circ}\text{C}$  the discharge frequency observed at 20 keV and a beam current density of  $40 \text{ nA/cm}^2$  was  $15 \text{ min}^{-1}$ . After turn-on of illumination the discharges continue for about 2.5 min. This corresponds to a critical temperature of about  $-30^{\circ}\text{C}$ . After turn-off of illumination the discharges reoccur at a sample temperature of about  $+15^{\circ}\text{C}$ .

This result, although qualitatively showing the expected delay for ceasing of discharge, is quantitatively in contradiction to the results obtained without cooling where the critical temperature for ceasing of discharge had been found to be between  $20^{\circ}\text{C}$  and about  $50^{\circ}\text{C}$ . It appears that in the presence of solar illumination the critical temperature is reduced by about  $60-70^{\circ}\text{C}$ .

This was confirmed by another test. With the chamber walls again cooled down to liquid nitrogen temperatures, the solar simulator intensity was reduced step-wise. At 0.5 solar constant still no discharges were observed although the sample temperature was down to  $-1^{\circ}\text{C}$ . At 0.25 solar constant regular discharges occurred again. The sample temperature then was about  $-45^{\circ}\text{C}$ .

## 7. CONDUCTIVITY THROUGH THE SUBSTRATE AT HIGH ELECTRIC STRESS LEVELS

The leakage current to the solar cell module through the substrate under electron irradiation of the rearside was measured by connecting the solar cell module terminal leads in parallel to the input of an electrometer. The measurements were made at room temperature at a beam current density of  $90 \text{ mA/cm}^2$ . The beam energy was increased in 2 keV steps up to 16 keV. The results obtained in the dark are shown in Table 1, giving the equilibrium current after decay of the displacement current component. Between 1 and 5 keV positive current values were obtained indicating a secondary emission coefficient of more than 1. At higher voltages the leakage current increases supralinearly which shows that the conductivity increases with voltage.

Illumination has a considerable influence on the leakage current. At 16 keV the current increases from  $-2.25 \mu\text{A}$  to  $-5.8 \mu\text{A}$  after turn-on of the solar simulator. (The cell gaps were not covered by a mesh during these measurements but still the light intensity at the rearside is only a small fraction of 1 S.C.) These results are qualitatively in agreement with the results recently obtained at Stanford Research Institute, SRI<sup>2</sup> on pure kapton samples. At SRI a conductivity increase of  $10^5$  was observed when illuminating kapton-H film with 2.3 suns of Xenon illumination.

Table 1. Current Through Sample versus Beam Voltage

$U = 0 \text{ kV}$	$j = 0 \text{ nA}$
$2 \text{ kV}$	$+40 \dots +20 \text{ nA}$
(Maximum bel ctwa $3 \text{ kV}$ )	
$4 \text{ kV}$	$+25 \dots +15 \text{ nA}$
$6 \text{ kV}$	$-30 \text{ nA}$
$8 \text{ kV}$	$-120 \text{ nA}$
$10 \text{ kV}$	$-260 \text{ nA}$
$12 \text{ kV}$	$-560 \text{ nA}$
$14 \text{ kV}$	$-1, 12 \mu\text{A}$
$16 \text{ kV}$	$-2, 25 \mu\text{A}$

## 8. IMPACT OF ELECTROSTATIC DISCHARGES ON THE ARRAY EXPERIMENT ELECTRONICS UNIT

In normal operation the array experiment electronics unit (AEE) is used to monitor the I-V curve of the test patch at six points and the array temperature at five locations on the solar array. Details of the design, construction, and performance of the AEE can be found in Ansorge and Plischel.<sup>3</sup>

The AEE telemetry sample sequence is shown in Table 2.

For the purpose of the test, only the current and voltage sensing terminals of the AEE engineering unit and the wiring for two temperature sensors were connected to the test sample in the simulation chamber. The remaining input terminals were connected to the check-out unit which also provided the power supply and the clock signal.

A print-out of AEE/test patch data is shown in Figure 8 indicating an open circuit voltage of 4.75 volts and a short circuit current of 263 mA with the test patch under 1 S.C. illumination. With the AEE running continuously, the electron beam voltage was increased in steps of 1 kV starting at zero.

Up to 17 kV no discharges and no anomalies of the AEE performance were observed. Slightly above 17 kV still no discharges were observed, either visually or with the detecting antenna, but the AEE output showed loss of clock synchronization. The AEE switched to the next channel at random rate.

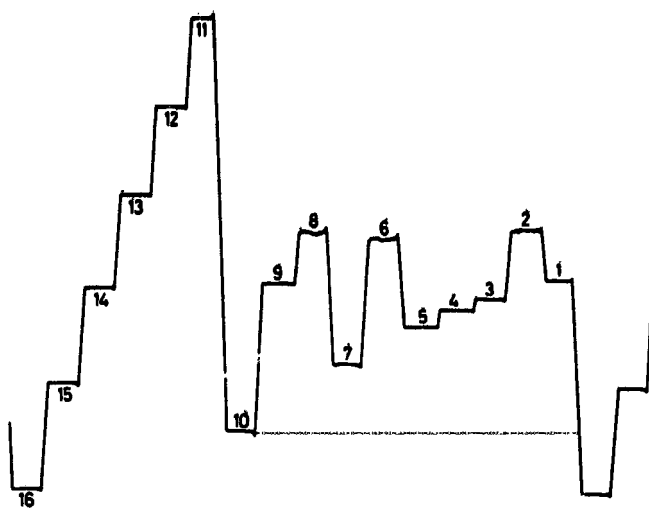
In order to obtain discharges, the solar simulation was turned off with the electron beam being kept at 17 kV. After 25 discharges, the solar simulation was turned on again and the electron beam was switched off. The AEE output at this stage is shown in Figure 9. The AEE samples only open circuit voltage values and zero current instead of the actual pairs of I/V values on the curve. This indicates

Table 2. AEF Sample Sequence

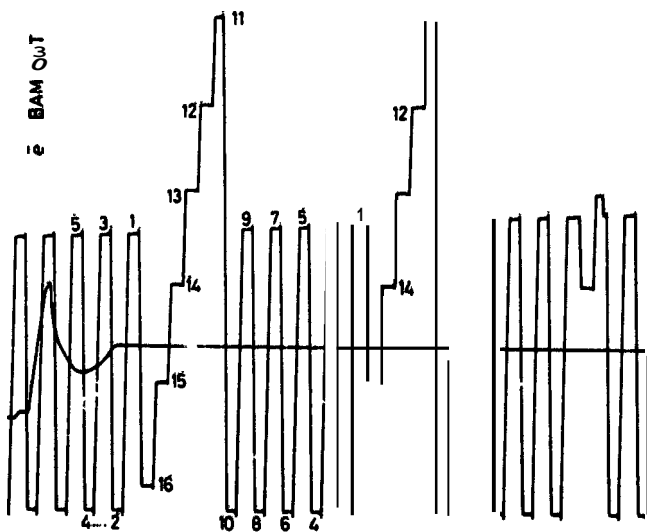
NO.	Nomenclature	
	Channel A	Channel B
1	$V_{oc}^*$	T1
2	$I_{sc}$	T1
3	$V_3$	T1
4	$I_3$	T1
5	$V_2$	TL
6	$I_1$	T1
7	$V_1$	T1
8	$I_1$	T1
9	$V_4$	T1
10	$I_4$	T1
11	$V_{ref}$	<100 mV
12	$T_1$	<100 mV
13	$T_2$	<100 mV
14	$T_3$	<100 mV
15	$T_4$	<100 mV
16	$T_5$	<100 mV

\*  $V_{oc}$  = open circuit voltage  
 $I_{sc}$  = short circuit current

that the input transistor(s) which load(s) the test patch according to the sample sequence has an open circuit failure.



**Figure 8. AEE Sample Sequence before Discharge**



**Figure 9. AEE Sample Sequence after Discharge**

## 9. CONCLUSIONS

Several new phenomena have been observed in this series of substorm charging tests that may lead to a better understanding of the in-flight behavior of the CTS solar array experiment. Moreover, the test results may be of general importance for other solar arrays of similar design.

Discharges due to electrostatic charging of the solar cell test patch rear side occur at energies above 15 keV when the front side of the test patch is not sun-illuminated. After turn-on of solar simulation, the discharge frequency decreases to zero within a short time. It could be shown that the test patch temperature is an important parameter for the discharge frequency. Above 30°-40°C no discharges are obtained. Moreover, the illumination level on the front side was shown to have an influence on the temperature limit below which discharges are obtained.

Finally it was shown that the experiment's electronics will not survive discharges in the test patch area. As the solar array experiment is still operating in space, it can be concluded that up to now no severe discharges have occurred in the test patch area. The conclusion is made plausible by the observed discharge frequency dependence on temperature and illumination.

The phenomenological nature of the tests does not allow more quantitative conclusions to be drawn. More detailed data, however, are needed for the design and the specification of future solar arrays. Therefore it is planned to continue the tests as soon as possible and to obtain quantitative results in the following areas:

- (1) Dependence of discharge energy, spectrum and frequency on the sample size.
- (2) Investigation of the temperature and illumination intensity dependence of charging/discharging phenomena,
- (3) Investigation of the behavior of new solar array substrate materials (For example, carbon-fiber-kapton compound) in a substorm environment.

## References

1. Stevens, N. Y., Lovell, R., and Gore, V. (1975) Spacecraft Charging Investigation for the CTS Project, NASA-TMX-71795,
2. Coffey, H. T., Nanewick, J. E., and Adams, R. C. (1975) Photoconductivity of High Voltage Space Insulating Materials, SRI Final Report For Contract NAS3-18912,
3. Ansorge, W., and Plischel, H. G. (1975) Final Report on the Array Experiment Electronics - AEE RFE Report.